## RESEARCH OF HIGH – ENERGY MILLING OF THE TiH<sub>2</sub>-BN POWDERS IN NITROGEN

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The system  $TiN+TiB_2$  is considered promising for creation of cutting tools with superior mechanical properties, such as hardness, fracture toughness, bend strength and wear resistance [1, 2].

Present study aimed at optimization of high-energy milling process of TiH<sub>2</sub>+BN mixtures in nitrogen for reaction-driven consolidation of dense ceramic composite based on TiN and TiB<sub>2</sub>.

Two types of titanium hydride  $TiH_2$  and  $TiH_x$  were used, which have been reduced by magnesium and obtained by affinage technique, respectivly. They differs by quantity of impurities and crystallography [3].  $TiH_2$  has face-centered cubic lattice ( $CaF_2$  – type structure),  $TiH_x$  - face-centered tetragonal lattice, which indicates that the last one has higher capacity of hydrogen [3].

Table.1 Properties of starting and milled of the powders and the mixtures.

D 1	TVDD*		1		-
Powder	$XRD^*$	S,	$d_{m,}$	Ο,	Fe,
	results	$m^2/g$	nm	wt.	wt.%
				%	
TiH <sub>x</sub>	TiH <sub>2</sub> tetr.	0,233	8310	0,1	0,038
				3	
TiH <sub>2</sub>	TiH <sub>2</sub> cub.	0,225	7050	0,1	0,25
				2	
BN	BN+B <sub>2</sub> O <sub>3s</sub>	2,82	930	5,4	0,034
				0	
TiH <sub>x</sub> +	TiH <sub>2</sub> +BN <sub>w</sub>	3,63	580	1,5	0,48
BN (1')				5	
TiH <sub>x</sub> +	TiH <sub>2</sub> +BN <sub>w</sub>	10,81	190	1,6	1,03
BN (5')	+TiB <sub>2 vw</sub>				
TiH <sub>x</sub> +	TiH <sub>2</sub> +BN <sub>v</sub>	15,00	140	3,6	2,25
BN(20')	w.+TiB <sub>2 w</sub>				
TiH <sub>2</sub> +	TiH <sub>2</sub> +	3,44	540	1,8	0,4
BN (1')	$\mathrm{BN}_{\mathrm{w}}$			6	
TiH <sub>2</sub> +	TiH <sub>2</sub> +BN <sub>v</sub>	10,54	173	2,1	0,76
BN (5')	w.+TiB <sub>2vw</sub>			1	
TiH <sub>2</sub> +	TiH <sub>2</sub> +TiB <sub>2</sub>	12,34	150	4,5	1,37
BN(20')	w			7	

\*s – strong; w – weak peaks; vw – very weak peaks.

Properties of starting and milled powders and the mixtures are shown in Table 1. X-ray diffraction analysis (XRD) of boron nitride showed strong peaks of  $B_2O_3$  (Table.1). The proportion between  $TiH_2$  ( $TiH_x$ ) and BN is 74,9:25,1, corresponds to stochiometric composition of the reagents in the reaction:

$$TiH_2 + BN = 2/3TiN + 1/3TiB_2$$
 (1)

Filling of the ball-mills with nitrogen was carried out under pressure of P=0,2 kPa for t=10min. The milling was made in planetary ball mill for 1, 5, and 20 min. Determination of the specific surface area was implemented by method low-temperature adsorption of nitrogen (BET). The average size of particles was calculated from the specific surface area suggesting spherical shape of particles [4], by formula:

$$d_{\rm m}=6/(S\cdot\gamma)$$
, (2)

where:  $d_m$ - average size particles,  $\mu m$ ; S- specific surface area of powder,  $m^2/g$ ;  $\gamma$ -density of material,  $g/cm^3$ .

After milling for 1 min. the phase composition corresponded to initial one in fact. X-ray diffraction analysis (XRD) shows, that the phase composition changes after milling during 5-20 min. Thus, intensity of peaks for boron nitride decreases as a result of amorphization [5]. After 5-20 min. of milling, the mechano-chemical synthesis of TiB<sub>2</sub> was revealed. Table 1 shows, that as a result of milling for 5-20 min. significant oxidizing and pollution with iron occurs.

Results of the investigations of the specific area surface dependence on milling time are shown on Fig.1. The intensive increase of the specific surface area was observed for 1-5 min. of milling. But growth of specific surface area is not so significant, as the last one, under increasing of milling time up to 20 min (Fig.1).

Investigations of the particle-size distribution were implemented by sedimentation analysis in terms of laser light scattering on device Zetasizer 1000HS. The 0,1% hexametaphosphate natrium solution in distilled water was chosen as a dispersion medium.

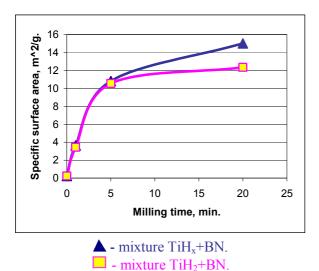


Fig.1. Dependence of specific surface area on milling time.

Table.2 Results of the particle-size distribution investigations of initial and milled powders.

	d <sub>mean.log.</sub>	by intensity.		by volume	
Powder	nm.	nu	scatteri	nu	scatte
		mb.	ng,	mb.	ring,
		pea	nm.	pea	nm.
		ks		ks	
BN	455	2	40,5-	3	32,2-
			5107		6430
TiH <sub>x</sub> +	272	1	38-	3	31-
BN (1')			3056		3848
TiH <sub>x</sub> +	226	1	20,1-	3	16-
BN (5')			801		801
TiH <sub>x</sub> +	192	1	22- 541	3	17-
BN(20')					681
TiH <sub>2</sub> +	291	2	26-	4	21-
BN (1')			3264		4110
TiH <sub>2</sub> +	233	2	107-	2	90-
BN (5')			494		585
TiH <sub>2</sub> +	181	2	79- 279	2	69-
BN(20')					321

Tabl.2 shows results of these investigations, which reveal, that the dispersion of powder BN takes place even after milling for 1 min. Increasing of

milling time leads to narrowing of particle-size distribution. Magnitude of  $d_{mean.\ log.}$  is average value of log-normal particle-sizes distribution.

Using the particle-size distribution in volume was caused by necessity of refinement of data on particle-size distribution in intensity according to Mie theory [6]. Therefore, as Table 2 shows, particle-size distribution in volume, as a rule, has higher modality and wider region of particle-size distribution. Sizes of starting powders particles, and also after milling for 1 min., have different magnitudes after specific surface definition and sedimentation analysis, that is bounded up with complex shape of particles surface of these powders. Increase of milling time leads to spheroidizing of particles shape.

Thus, high-energy milling for 1 min. is optimal at these conditions, as a consequence of that powder mixture with specific surface 3,44-3,63 m<sup>2</sup>/g, oxygen contents 1,55-1,86 %wt., iron contents 0,40-0,48 %wt. is obtained.

## References

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